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## Humanoid Dynamic Controller

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### Abstract

*In the last years several investigators have focused on the development and control of humanoid robots able to acquire human behaviors and features, in order to be able to interact with humans and work together with them. The fall of a humanoid robot can lead to damages, which entail costs for repair or even human health risks, so ensuring stability is a main concern in terms of cost and safety. This document presents the implementation of a dynamic controller for humanoid robots, able to position the robot's center of mass in a certain location operating as a stability module. It is also described a precise behavior of preparing an omnidirectional kick for a humanoid robot by placing the support foot in a precise position and orientation calculated in accordance with the robot's position, the ball and the target, and by transferring the robot's center of mass to the desired position.*

**Keywords:** Humanoid Stability; Dynamic Controller; Prepare Kick.

### 1. Introduction

In the last two decades, the area of humanoid robotics has shown significant improvements. This evolution results from the development of new actuators, computers and other technologies that make possible the construction of a machine with human-like skills. Since 1960 the robotics industry has been growing and so has been the research in this area where several universities such as Waseda University [1] and Tokyo, and companies like Honda [2], Boston Dynamics and Aldebaran Robotics [3] have done research work.

The main purpose in the humanoid robots research is to allow the robots to have the ability to work together with humans due to their flexibility and adaptability that allow them to use human tools and human environments. However, it is necessary to ensure the safety of both human and robots.

The control theory is a branch of engineering with the aim of controlling a dynamic system through its inputs. The application of these controllers is extended to large areas, including robotics, where they are frequently used to control the servo motors and in stability modules. In engineering, a control system has at least two main modules, the controller itself and the system to be controlled. A stability module is essential for humanoid robot's stability using a dynamic controller to achieve the desired set points [4]. The proposed controller objective is to keep the robot statically stable, positioning the center of mass in a desired set point to ensure the robot's stability during precise movements.

The work described in this article was developed in the scope of the Portuguese soccer team FCPortugal, competing in the world's RoboCup 3D Simulation League and Standard Platform League [5-8], in order to reach a behavior combined with others previously developed [9-10] to equip a humanoid robot with the ability to kick a ball in various directions, perform a kick/pass without the preparation phase, and maintaining the humanoid body stability, creating a team of NAO robots [3], real or virtual, with the capability to play a soccer match decently.

## 2. The Center of Mass Dynamic Controller

The developed controller allows the use of various controlling architectures to control the projection of the center of mass (CoM) on the ground through a PID controller. All the developed control methods were adjusted according to the Ziegler Nichols heuristic method [11].

### 2.1. The arms

Since the robot arms during a football match are rarely used, it was initially developed a controller that uses the robot arms to position the center of mass.

The proposed module uses a PID controller that receives the error position of the center of mass  $(x, y)$  relative to the robot's shoulder and calculates the desired position for the robot arms  $(x, y)$ . As for purposes of stability, the position of the arm should be as close as possible to the support plane, the  $z$  coordinate of the arms is the lowest in the robot workspace and can be calculated from the length of the arm and the position  $(x, y)$  with:

$$z = -\sqrt{l_{\text{arm}}^2 + x^2 + y^2} \quad (2.1)$$

The coordinates obtained in equation 2.1 are then applied to the inverse kinematics module to place the robot arm in the desired position controlling the robot's center of mass.

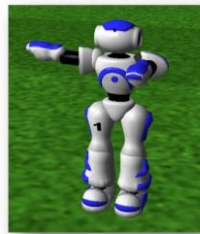


Figure 2.1. Projection of the robot arm along the  $y$  axis

Applying the pose illustrated in Figure 2.1 the position of the center of mass of the robot has the response shown in Figure 2.2.

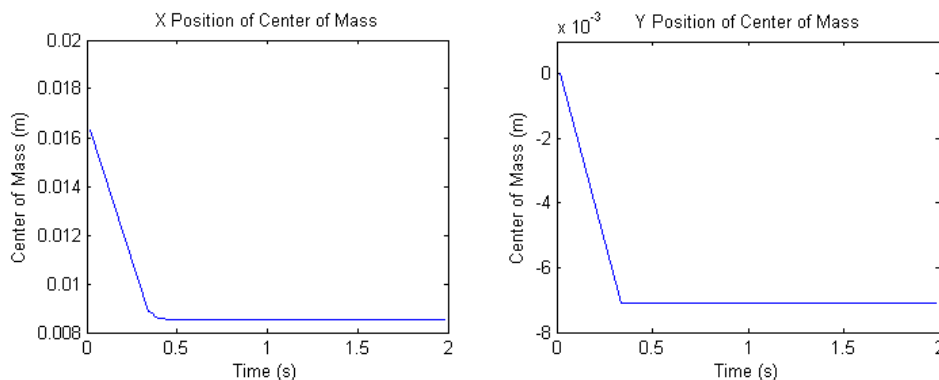


Figure 2.2. Robot's CoM response

This method has proved to be ineffective in controlling the position of the robot's center of mass because the robot arms mass is too small relative to its total mass [3] and therefore the center of mass manipulability with this method is very low. In Figure 2.2 it can be seen that the arm can only change the robot's center of mass position for about 9 mm in the  $xy$  plane.

### 2.2. The legs

To control robot's center of mass position, the robot's phase of movement must be taken into account. Figure 2.3 represents the phases of humanoid locomotion.

As can be seen, the phases "a" and "c" correspond to the double support phase, in which both feet are in contact with the ground, and the phases "b" and "d" correspond to single support phase in which only one foot is in contact with the ground.

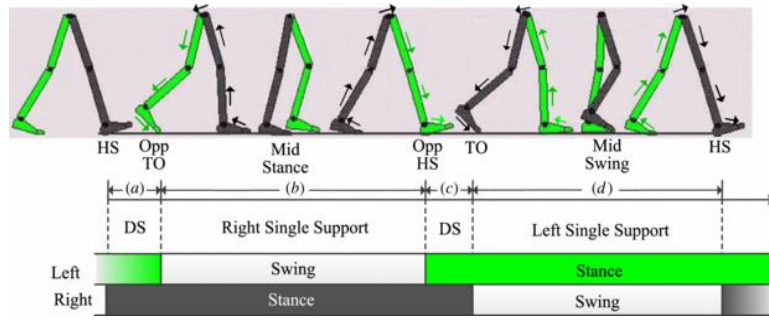


Figure 2.3. Phases of humanoid locomotion

**2.3. Double support phase**

In the double support phase pitch and roll of both foot and hip joints are used. Thus, using an angle between each pair of hip joints, and applying the opposite angle in the foot joints, the robot's body is moved parallel to the ground. This way we can control the x position of the robot through the pitch angle applied to the robot's foot and hip joints, and we can control the y position of the robot through the roll angle applied to the robot's foot and hip joints. This control method is shown in Figure 2.4.

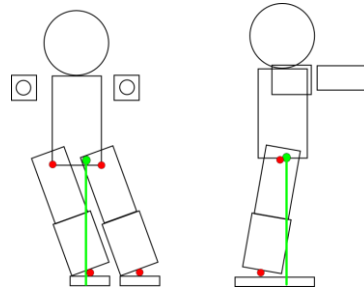


Figure 2.4. Controlling the robot's center of mass in double support phase

Figure 2.5 shows the response of the controller after the application of a square wave input ranging from the position (0, 0) to (-0.05, -0.02), in meters, with a 6 seconds period. Analyzing the response we can verify that the system presents an under damped response with low rise and settling times. This analysis demonstrates that the controller is accurate and ideal for situations that require an exact positioning of the robot's center of mass.

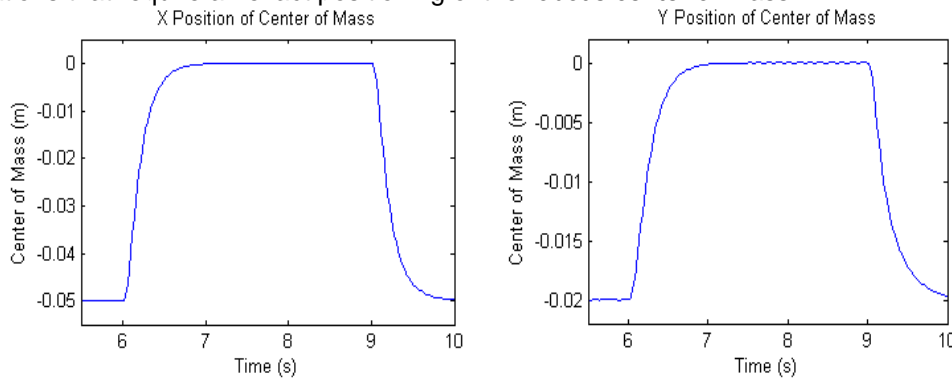


Figure 2.5. Position of the robot's center of mass being controlled in double support phase

**2.4. Single support phase**

In the single support phase we propose two different methods to control the robot's center of mass position. We can use only the hips pitch and roll joints, and then we can position the robot's center of mass by changing the robot's torso orientation, or we can use both hip and foot joints just like in double support phase.

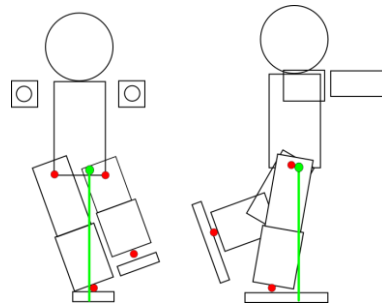


Figure 2.6. Controlling the robot's center of mass in single support phase with hip and foot joints.

As can be seen in Figure 2.6, by applying an angle determined by the PID controller to the robot's foot and hip joints, with the latter having opposite sign of the first, it is possible to move the robot's center of mass while maintaining the orientation of the trunk.

Figure 2.7 shows the response of the controller after the application of an input square wave ranging from the position (0, 0) to (-0.05, -0.02), in meters, with a 6 seconds period. Analyzing this figure we can verify that the system has an under damped response with low rise and settling times. This method's response is quite similar to the one presented by the double support phase due to their related features. This method is accurate and ideal for applications which require precise positioning of the robot's center of mass.

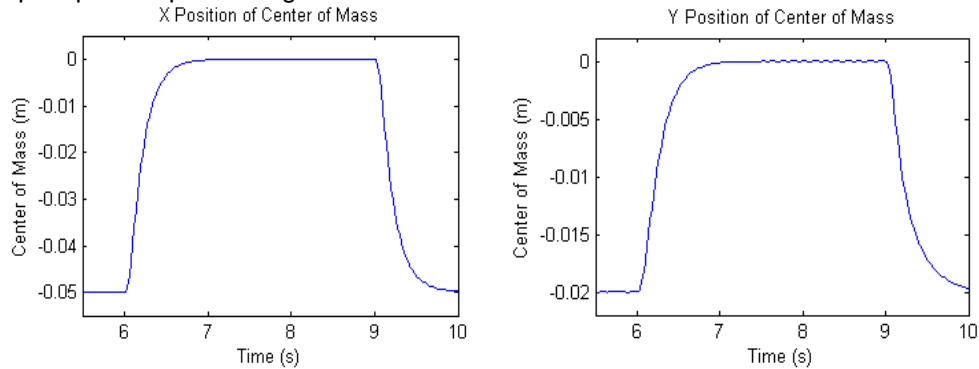


Figure 2.7. Position of the robot's center of mass being controlled in single support phase with foot and hip joints

The control sequence of the method mentioned above is shown in figure 2.8.

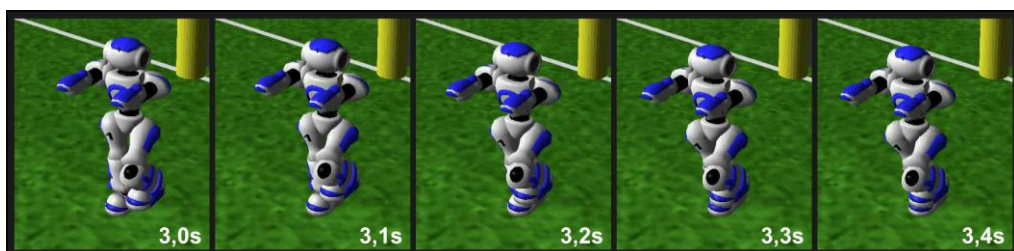


Figure 2.8. Control sequence of the robot's center of mass being controlled by the foot and hip joints in single support phase

As can be seen in figure 2.9, by applying an angle determined by the PID controller to the robot's hip joints we can move the robot's center of mass. Thus, the robot remaining joints are available to perform any task required by the robot's behavior. Using only two joints, this method is the least invasive way to control the robot's center of mass.

Figure 2.10 shows the response of the controller after the application of an input square wave ranging from the position (0, 0) to (-0.05, -0.02), in meters, with a 6 seconds period. By analyzing figure it is possible to verify that the system presents an over damped response with minimal rise time and low overshoot of approximately 5%. This control method is fast and

precise being suitable for situations which require fast positioning of the robot's center of mass as in case of robots balance.

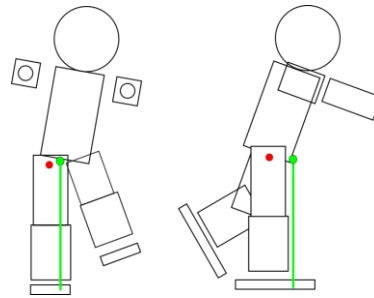


Figure 2.9. Controlling the robot's center of mass in single support phase with hip joints.

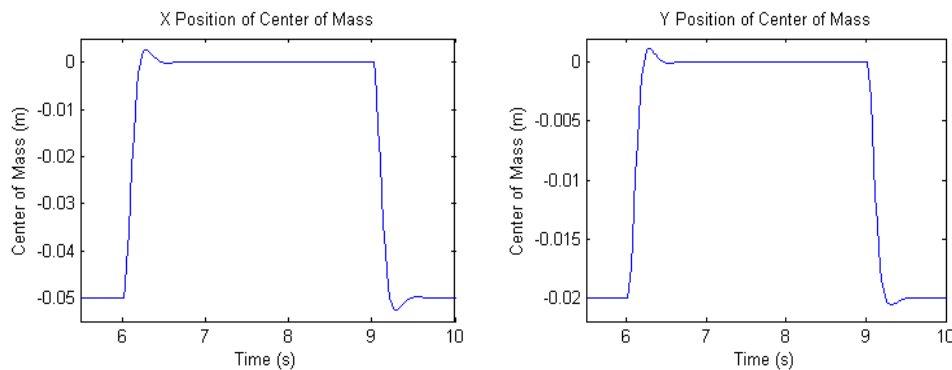


Figure 2.10. Position of the robot's center of mass being controlled in single support phase with hip joints

The control sequence of the method mentioned above is shown in figure 2.11.

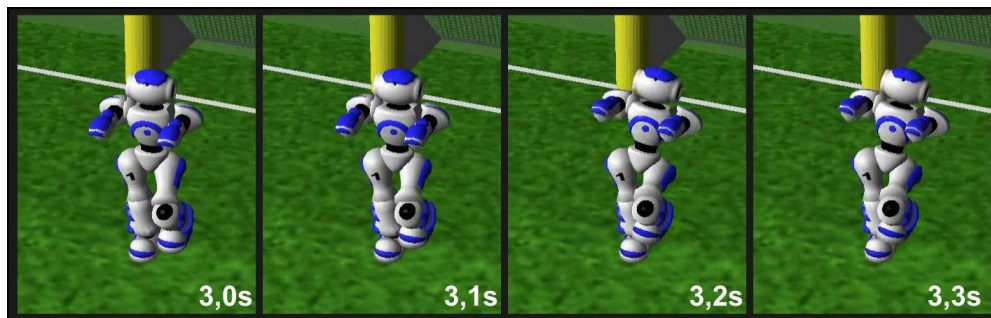


Figure 2.11. Control sequence of the robot's center of mass being controlled by the hip joints in single support phase

By overlaying the response of the method using hip and foot joints represented in figure 2.7, with the response of the method using only hip joints represented in figure 2.10, we obtained the graph presented in figure 2.12. We can observe that we can obtain a faster response using the hip joints method than using both joints, but the first one has an overshoot of nearly 5%. Thus, the hip and foot joints method should be used in situations which require the orientation of the trunk to remain constant during the movement or in applications where it isn't allowed overshoot, as in the precise positioning of the robot's center mass around the ends of the robot's support polygon. The method that only uses the hip joints should be used in all other situations and is especially suited for balance situations due to its fast response and the possibility of overshoot.

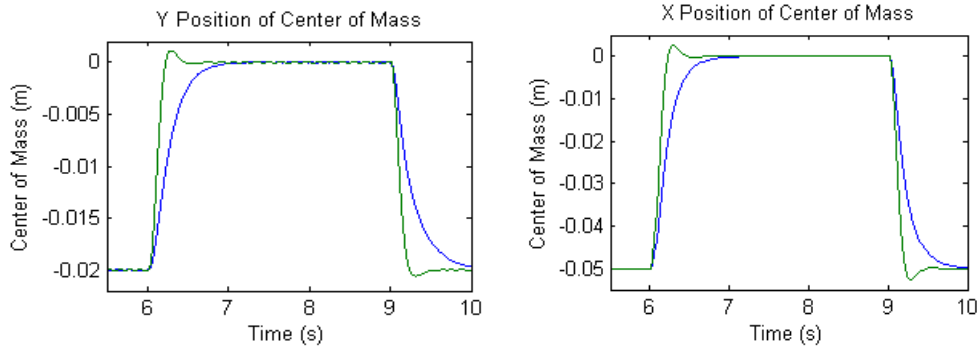


Figure 2.12. Comparison of response between the method that uses the hip and feet joints (blue) and the method that only uses the hip joints (green)

### 3. The Prepare Kick

#### 3.1. World analysis

In order to allow a dynamic and flexible prepare kick movement it is necessary to perform a world analysis and then calculate the exact support foot position for the kick's execution. Therefore, it is necessary to consider three objects:

- Player;
- Ball;
- Target.

Using these set of objects it is possible to calculate the foot position and orientation relative to the player using a set of parameters obtained by optimizing the best foot start position to the kick and relating the three objects mentioned. The parameters are:

- *dist* - Distance from the foot position to the ball;
- $\theta$  - Angle between the target and the foot position;
- $\alpha$  - Foot orientation relative to the target.

Initially, the target and ball coordinates are corrected according to the robot's orientation so they can be expressed according to the robot's frame. The figure 3.1 outlines the calculation of the position where the robot must place the support foot.

In this calculation is applied a rotation to the vector that goes from the target to the ball, in blue, of  $\theta$  and its length is normalized to *dist*. Thus, the point where the robot must put his foot is obtained through the sum of the vector that goes from the robot to the ball with the vector that goes from the ball to the support point, in red.

The foot orientation angle relative to the robot's initial pose is given by the sum of the angle formed between the ball and the target, with the angle  $\alpha$  given as a parameter.

#### 3.2. Motion planning

The implemented movement can be decomposed in five phases, being: transition from double support to single support, positioning the support foot, lowering the body, transferring the robot's center of mass and raise phase. Among these, the phases of positioning the support foot and lowering the body are performed in parallel.

##### 3.2.1. Transfer to single support

The strike movement preparation begins with the assumption that the robot is in a stable position in the phase of double support. This security can be obtained by analyzing the position of center of mass relative to the support polygon, as described in section 2. In order to perform a step, it is necessary to place the robot only supported by one leg, and for that the first stage of preparation consists in transferring the shot from the center of mass of the robot to the contact surface between the robot foot that will shoot and soil, then lifting the opposite foot.



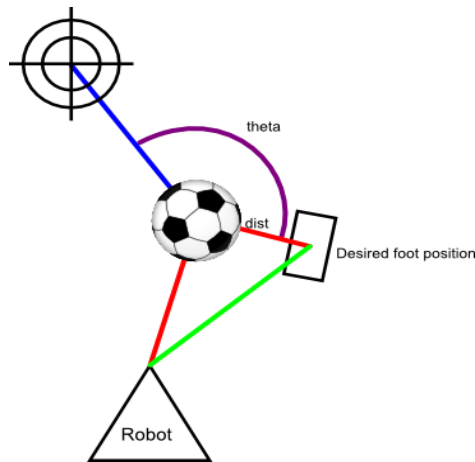


Figure 3.1. Calculation of the robot's support foot position

Figure 3.2 represents the robot transferring to single support.



Figure 3.2. Following transfer of the robot to single support

**3.2.2. Support foot placing**

Since the workload of the leg of the robot, shown in figure 3.3 by a semicircle in red, does not contain the end point of the foot support desired, represented in blue, the robot should set foot in the point whose projection in the semicircle  $z$  intersects representative of the workload. Thus, by lowering the foot opposite the robot places the support foot in the desired position. Thus, the stand follows a Bezier curve of degree 3 that will take the walk to this position in a circular path.

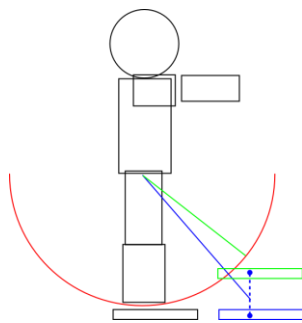


Figure 3.3. Robot's leg workload

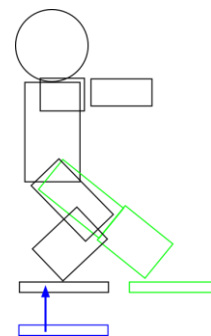


Figure 3.4. Robot's body lowering

**3.2.3. Robot's body lowering**

To put the kick foot in the desired position the robot will lower the body according to the elevation of the foot set in the previous paragraph and shown in Figure 3.4. The foot should follow a linear path down which ends when the robot returns to the position of double support.

The figure 3.5 represents the parallel execution of the lowering of the robot body and placing the foot support.



Figure 3.5. Sequence of the lowering and placing support foot

### 3.2.4. Transfer of the robot's center of mass

After lowering the robot it is necessary to transfer of center of mass of the robot from one foot to the other, to make possible the support of the robot's weight on the other foot. Since the position of the pelvis of the robot is kept within the working volume of both legs, it is possible to carry out a linear translation to the foot of same support required, as shown in Figure 3.6.

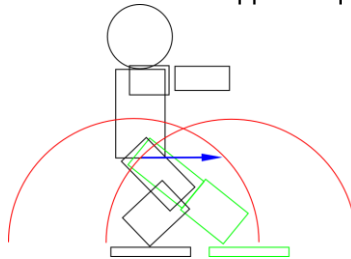


Figure 3.6. Transfer the robot's center of mass

The figure 3.7 represents the center of mass transfer of the robot.



Figure 3.7. Transfer the robot's center of mass

### 3.2.5. Kick's position

After the center of mass transferred, the kick foot can be placed on the robot pose desired shot, as shown in figure 3.8.

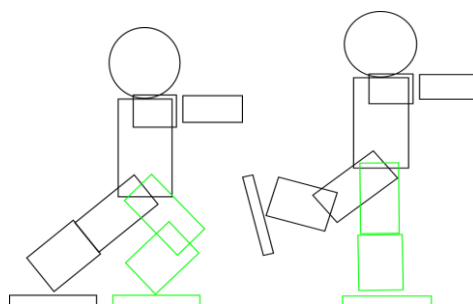


Figure 3.8. Pose after the final transfer of the center of mass of the robot pose and shot



Figure 3.9 represents several positions of the robot during kick's pose placing and kick.



Figure 3.9. Sequence of the kick's poses placing and respective kick

#### 4. Tests and results

The kick viable area was checked by performing several tests to the prepare kick movement. These tests consisted in positioning the robot in a set of predetermined positions and orientations relative to the ball and then verifying results in terms of distance and direction. Although the results obtained are subject to change, since the parameters defined in Section 3.1 can be changed through an optimization process, the ability to kick isn't as susceptible to these changes.

The area above the ball has been decomposed into a matrix with a resolution of 5 cm, in which the robot is positioned. This decomposition was carried out for a variation of x, (-0.25 and 0) meters, and y, (-0.25 and 0.25) meters. At each point of the matrix, angles between  $-50^\circ$  and  $50^\circ$  with intervals of  $10^\circ$  were tested and then two samples per test were made for results confirmation. To confirm the conditions that ensure the robot's ability to perform the prepare kick with his right foot, over 1300 tests were made and the results were analyzed with the MatLab tool. This analysis transformed the set of numbers into a gray scale image relating the distance traveled by the ball with the robot's initial pose.

The results after applying this transformation to all positions with the robot aligned with the target are shown in figure 4.1. In this figure, the white color represents a null distance and the black color represents a distance travelled by the ball of 18 meters.

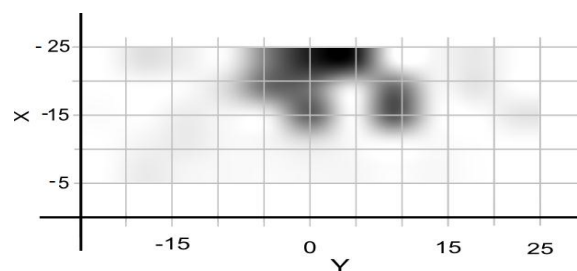


Figure 4.1. Representation of the kick distance relative to the robot's position when it is aligned with the target

The robot kick's performance is affected by the position where the movement was started, as presented in figure 4.1.

Being defined the minimum distance as 7 meters to consider that the robot is capable of performing a shot, by applying a binarization to the referred image with the appropriate threshold, there was thus obtained the shot area provided by the ability to move to the right foot. To obtain the area of capacity to strike with both feet, a union was made between representative

pictures of the results for a given orientation, with the mirror image of the representative results for the opposite orientation.

This result gave the following set of allowable shot areas according to the angle between the target and orientation of the player:

#### 4.1. Zero degree orientation

Figure 4.2 represents the permissible area of shot in relation to the robot's position while it is at an angle of  $0^\circ$  between its direction and the target. When the robot is aligned with the target, the allowable area is wide and has a set of very good results, with a maximum of 16.16 m recorded at position (-25, 5) cm. The two small areas of the shot recorded inadmissible at the bottom of the graph should overlap to the feet of the punch which makes it impossible to achieve. This approach is extremely favorable to the shot and has a vast area in which it is liable to be executed.

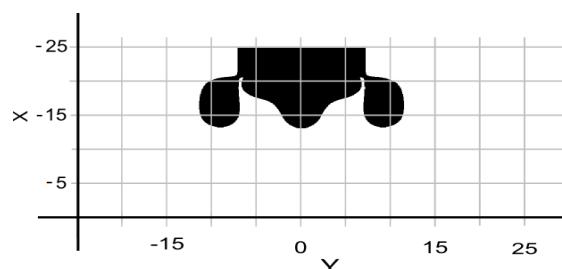


Figure 4.2. Representation of shooting allowable area from the position of the robot when it is at an angle of  $0^\circ$  between their direction and the target

#### 4.2. Ten degree orientation

Figure 4.3 represents the permissible area of shot in relation to the robot's position while it is at an angle of  $10^\circ$  between the orientation and the target.

When the robot encounters an orientation of 10 degrees to the target, the permissible area remains extensive in many ways similar to the previous one. This orientation is very favorable to the shot and has a vast area in which it is liable to be executed. In this orientation, the preparation of shot has a set of very good results with a maximum of 16.69 m recorded at position (-25, 0) cm.

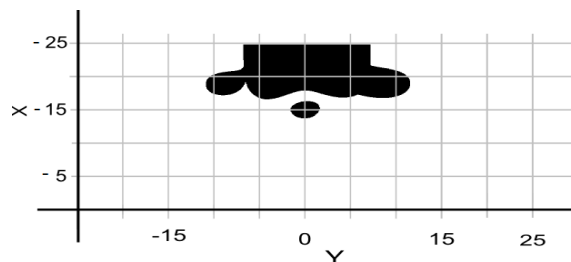


Figure 4.3. Representation of shooting allowable area from the position of the robot when it is at an angle of  $10^\circ$  between the orientation and the target

#### 4.3. Twenty degree orientation

The figure 4.4 represents the allowable shooting area in relation to the robot's position while it is at an angle of  $20^\circ$  between the orientation and the target.

When the robot encounters an orientation of 20 degrees to the target, the admissible area is the largest, enabling a set of tests performed with more than  $80\text{cm}^2$ . This approach is most favorable for the performance of the shot and has a set of excellent results with a maximum of 17.03 m recorded at position (-20, 5) cm.

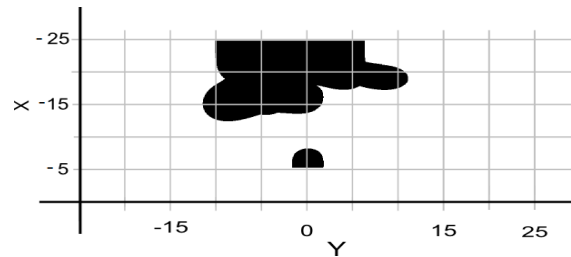


Figure 4.4. Representation of shooting allowable area from the position of the robot when it is at an angle of  $20^\circ$  between the orientation and the target

#### 4.4. Thirty degree orientation

The figure 4.5 represents the allowable shooting area in relation to the robot's position while it is at an angle of  $30^\circ$  between the orientation and the target.

When the robot encounters an orientation of  $30^\circ$  in relation to the target, the permissible area is slightly worse compared to previous results. Despite all, this approach has a number average results of up to 12.96 m recorded at position (-20, 0) cm.

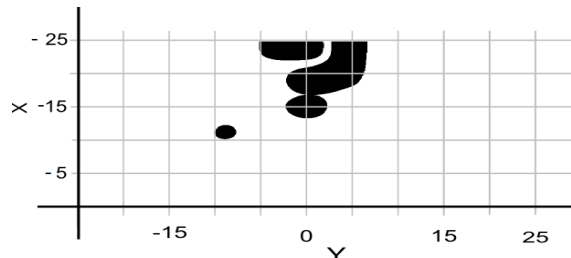


Figure 4.5. Representation of shooting allowable area from the position of the robot when it is at an angle of  $30^\circ$  between the orientation and the target

#### 4.5. Forty degree orientation

The figure 4.6 represents the allowable shooting area in relation to the robot's position while it is at an angle of  $40^\circ$  between the orientation and the target.

When the robot is in an orientation of  $40^\circ$  in relation to its target, the acceptable area is a bit worse in comparison with previous results, being considerably reduced. Despite all, this approach has a number of results with a maximum of 12.74 m recorded at position (-20, 0) cm.

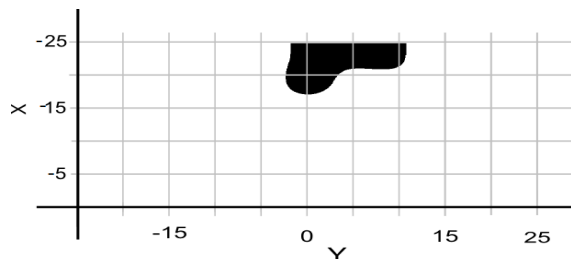


Figure 4.6. Representation of shooting allowable area from the position of the robot when it is at an angle of  $40^\circ$  between the orientation and the target

#### 4.6. Fifty degree orientation

The figure 4.7 represents the allowable shooting area in relation to the robot's position while it is at an angle of  $50^\circ$  between the orientation and the target. When the robot encounters an orientation of  $50^\circ$  in relation to the target, the allowable area for shot preparation is greatly reduced. Nevertheless, given the extremely unfavorable conditions in orientation of the robot, this configuration has a set of acceptable results with a maximum of 13.06 m recorded at position (-25, 10) cm.

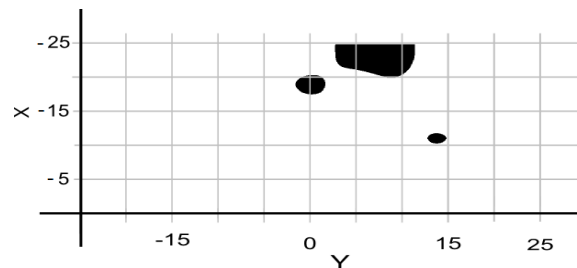


Figure 4.7. Representation of shooting allowable area from the position of the robot when it is at an angle of  $50^\circ$  between the orientation and the target

## 5. Conclusion

In this work, a stability humanoid dynamic controller and a kick preparation movement were described. The stability controller allows the equilibrium evaluation, the control of the position of the center of mass, and the choice of the appropriate control method related to the response desired for the robot, constituting a vital tool for the control and safety of the robot and also a tool for evaluating and optimizing behavior.

Based on the stability module it was possible to develop a behavior for an omnidirectional kick preparation, providing a sequence for a single shot. An extensive set of tests proved the robustness and flexibility of the developed movement.

The parameters used on these tests were hand tuned. Future work will consist in optimizing the parameters of the behavior of kick preparation for multiple sets of kicks, in developing a method of omnidirectional locomotion based on defined locomotion behavior, and incorporation of kick preparation on a stepping movement.

## Acknowledgements

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